

Velocity calibration and wavefield decomposition for walkover VSP data

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Finite-offset (FO) 2D CRS stack theory initially introduced for surface seismic (Zhang et al., 2001)

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- ▶ second order approximation based on paraxial ray-theory

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- ▶ second order approximation based on paraxial ray-theory
- ▶ central ray is non-zero offset

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 - expansion points (\vec{x}_S, \vec{x}_G) for each simulated source and receiver pair

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 - ▶ expansion points (\vec{x}_S, \vec{x}_G) for each simulated source and receiver pair
- ▶ FO CRS operator depends on five parameters

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 - multi-dimensional optimization problem

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- ▶ geometrical explanation of stacking parameters

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 - ▶ hypothetical wavefronts, in vicinity of sources and receivers assuming:

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 - ▶ local isotropy

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 - ▶ known velocities

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- ▶ FO CRS operator depends on five parameters
 - multi-dimensional optimization problem
- ▶ geometrical explanation of stacking parameters
 - hypothetical wavefronts, in vicinity of sources and receivers assuming:
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 - ▶ known velocities → calibration required

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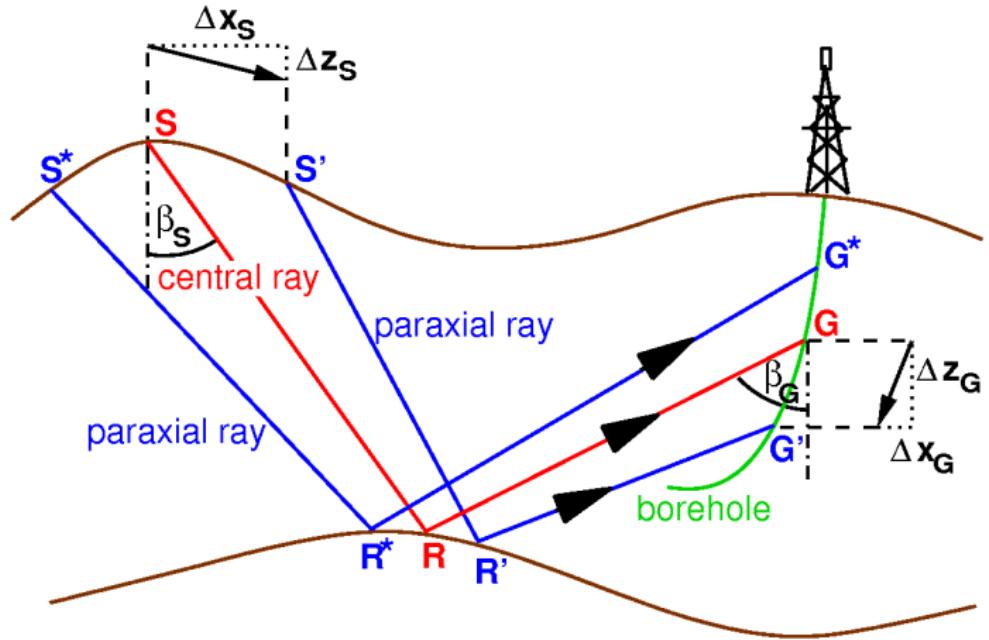
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VSP measurement configuration

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S and G are the positions of \vec{x}_S and \vec{x}_G , respectively



CRS Operator for arbitrary geometry

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$$\begin{aligned}\tau_{\text{hyp}}^2 &= \left(\tau_0 + \frac{\sin \beta_S}{v_S} \Delta x_S - \frac{\cos \beta_S}{v_S} \Delta z_S + \frac{\sin \beta_G}{v_G} \Delta x_G - \frac{\cos \beta_G}{v_G} \Delta z_G \right)^2 \\ &\quad + \tau_0 AB^{-1} (\Delta x_S - \Delta z_S \tan \beta_S)^2 \\ &\quad + \tau_0 DB^{-1} (\Delta x_G - \Delta z_G \tan \beta_G)^2 \\ &\quad - 2 \tau_0 B^{-1} (\Delta x_S - \Delta z_S \tan \beta_S) (\Delta x_G - \Delta z_G \tan \beta_G).\end{aligned}$$

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- ▶ τ_0 : traveltime of central FO ray

CRS Operator for arbitrary geometry

$$\begin{aligned}\tau_{\text{hyp}}^2 = & \left(\tau_0 + \frac{\sin \beta_S}{v_S} \Delta x_S - \frac{\cos \beta_S}{v_S} \Delta z_S + \frac{\sin \beta_G}{v_G} \Delta x_G - \frac{\cos \beta_G}{v_G} \Delta z_G \right)^2 \\ & + \tau_0 AB^{-1} (\Delta x_S - \Delta z_S \tan \beta_S)^2 \\ & + \tau_0 DB^{-1} (\Delta x_G - \Delta z_G \tan \beta_G)^2 \\ & - 2 \tau_0 B^{-1} (\Delta x_S - \Delta z_S \tan \beta_S) (\Delta x_G - \Delta z_G \tan \beta_G).\end{aligned}$$

- ▶ τ_0 : traveltimes of central FO ray
- ▶ $\Delta x_S, \Delta z_S, \Delta x_G, \Delta z_G$: horizontal and vertical offsets

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- ▶ τ_0 : traveltime of central FO ray
- ▶ $\Delta x_S, \Delta z_S, \Delta x_G, \Delta z_G$: horizontal and vertical offsets
- ▶ v_S, v_G : velocities in the vicinity of \vec{x}_S and \vec{x}_G

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- ▶ τ_0 : traveltime of central FO ray
- ▶ $\Delta x_S, \Delta z_S, \Delta x_G, \Delta z_G$: horizontal and vertical offsets
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- ▶ β_S, β_G : emergence angles of central ray

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$$\begin{aligned}\tau_{\text{hyp}}^2 = & \left(\tau_0 + \frac{\sin \beta_S}{v_S} \Delta x_S - \frac{\cos \beta_S}{v_S} \Delta z_S + \frac{\sin \beta_G}{v_G} \Delta x_G - \frac{\cos \beta_G}{v_G} \Delta z_G \right)^2 \\ & + \tau_0 \textcolor{brown}{AB}^{-1} (\Delta x_S - \Delta z_S \tan \beta_S)^2 \\ & + \tau_0 \textcolor{violet}{DB}^{-1} (\Delta x_G - \Delta z_G \tan \beta_G)^2 \\ & - 2 \tau_0 \textcolor{blue}{B}^{-1} (\Delta x_S - \Delta z_S \tan \beta_S) (\Delta x_G - \Delta z_G \tan \beta_G).\end{aligned}$$

- ▶ τ_0 : traveltime of central FO ray
- ▶ $\Delta x_S, \Delta z_S, \Delta x_G, \Delta z_G$: horizontal and vertical offsets
- ▶ v_S, v_G : velocities in the vicinity of \vec{x}_S and \vec{x}_G
- ▶ β_S, β_G : emergence angles of central ray
- ▶ $\textcolor{violet}{DB}^{-1}, \textcolor{brown}{AB}^{-1}, \textcolor{blue}{B}^{-1}$: composites of elements of ray-propagator matrix

A look at multi-coverage walkover data

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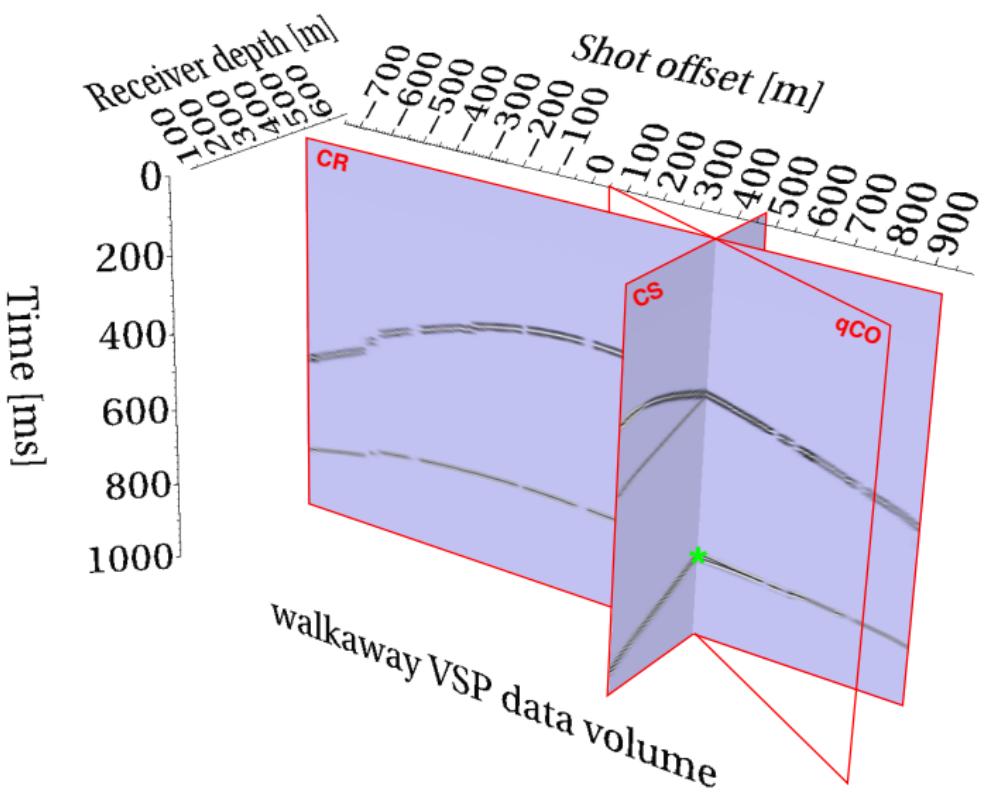
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Stacking parameters are converted to wavefield
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- ▶ inaccurate velocities \Leftrightarrow incorrect attributes

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- ▶ inaccurate velocities \Leftrightarrow incorrect attributes
- ▶ conventional way: checkshot inversion

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- ▶ inaccurate velocities \Leftrightarrow incorrect attributes
- ▶ conventional way: checkshot inversion often too inaccurate!
- ▶ alternatively: CRS analysis of downgoing waves

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Assumption:

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Assumption:

- ▶ velocities virtually constant within paraxial vicinity

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Assumption:

- ▶ velocities virtually constant within paraxial vicinity (already inherent assumption of CRS method)

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Assumption:

- ▶ velocities virtually constant within paraxial vicinity (already inherent assumption of CRS method)
- ▶ length of slowness vector $|\vec{p}|$ independent of incidence angle

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- ▶ VSP data provides only one slowness component:

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- ▶ VSP data provides only one slowness component:
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- ▶ VSP data provides only one slowness component:
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 - ➡ in general insufficient to determine $|\vec{p}|$

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- ▶ VSP data provides only one slowness component:
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- ▶ special case: walkover VSP

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- ▶ special case: walkover VSP
 - ▶ p_t of downgoing rays varies with source position \vec{x}_S

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- ▶ special case: walkover VSP
 - ▶ p_t of downgoing rays varies with source position \vec{x}_S
 - ▶ a ray tangent to well at receiver \vec{x}_G is very likely

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 - ▶ a ray tangent to well at receiver \vec{x}_G is very likely there: naturally $p_t \equiv |\vec{p}|$

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- ▶ Strategy

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- ▶ Strategy
 - ▶ identify downgoing direct P and/or S arrivals

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- ▶ Strategy
 - ▶ identify downgoing direct P and/or S arrivals
 - ▶ calculate $p_t(\vec{x}_S, \vec{x}_G)$ \forall sources S and receivers G

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- ▶ Strategy
 - ▶ identify downgoing direct P and/or S arrivals
 - ▶ calculate $p_t(\vec{x}_S, \vec{x}_G)$ \forall sources S and receivers G
 - ▶ for each G , search maximum of $p_t(\vec{x}_S, \vec{x}_G = \text{const})$

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- ▶ Strategy
 - ▶ identify downgoing direct P and/or S arrivals
 - ▶ calculate $p_t(\vec{x}_S, \vec{x}_G)$ \forall sources S and receivers G
 - ▶ for each G , search maximum of $p_t(\vec{x}_S, \vec{x}_G = \text{const})$
 - ➡ searched-for velocity $v(\vec{x}_G) = \max \{p_t(\vec{x}_S; \vec{x}_G)\}^{-1}$

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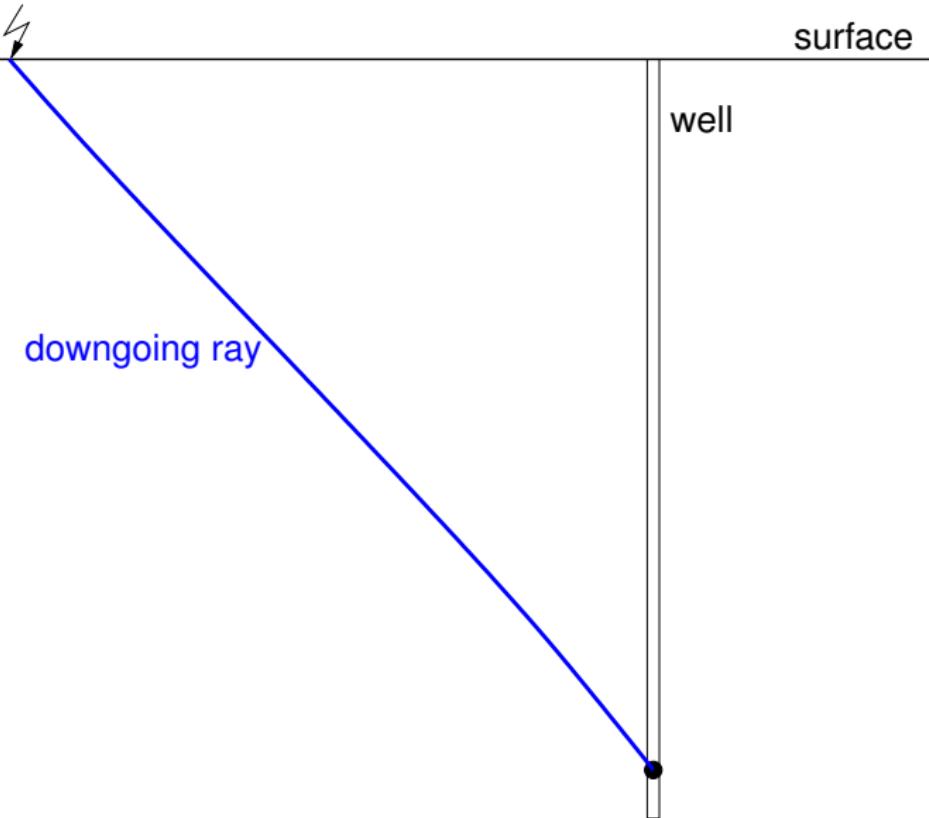
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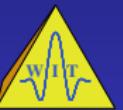
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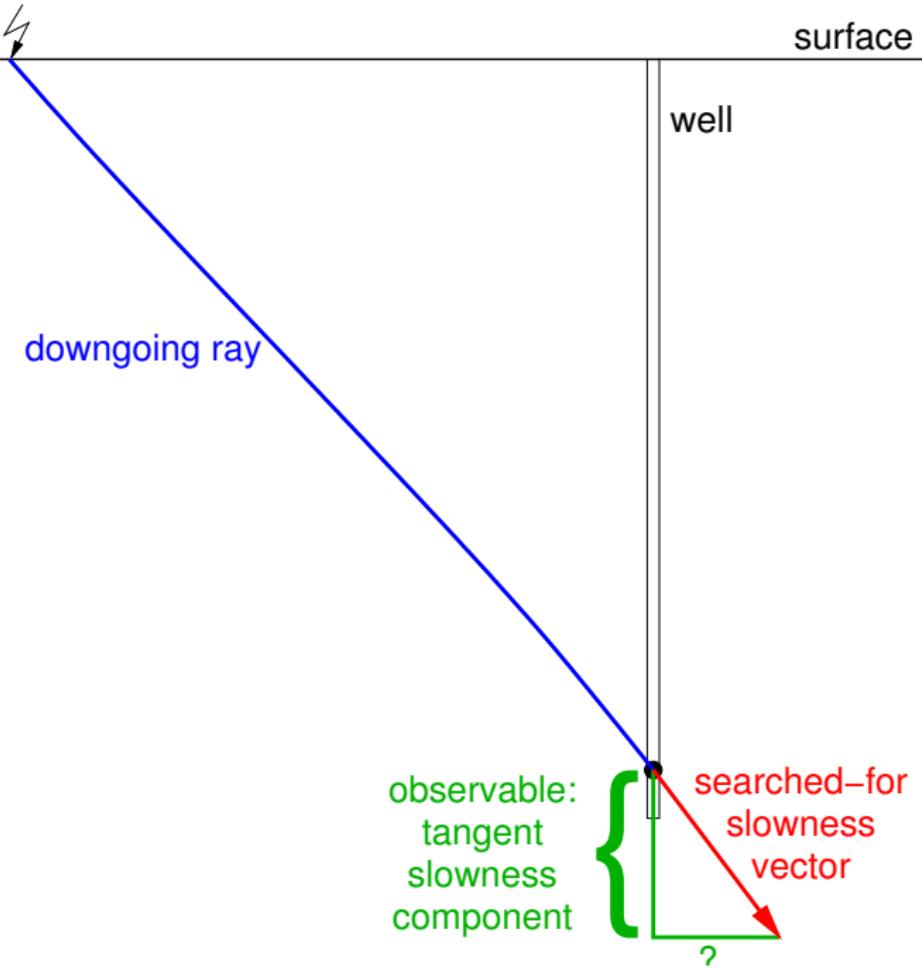
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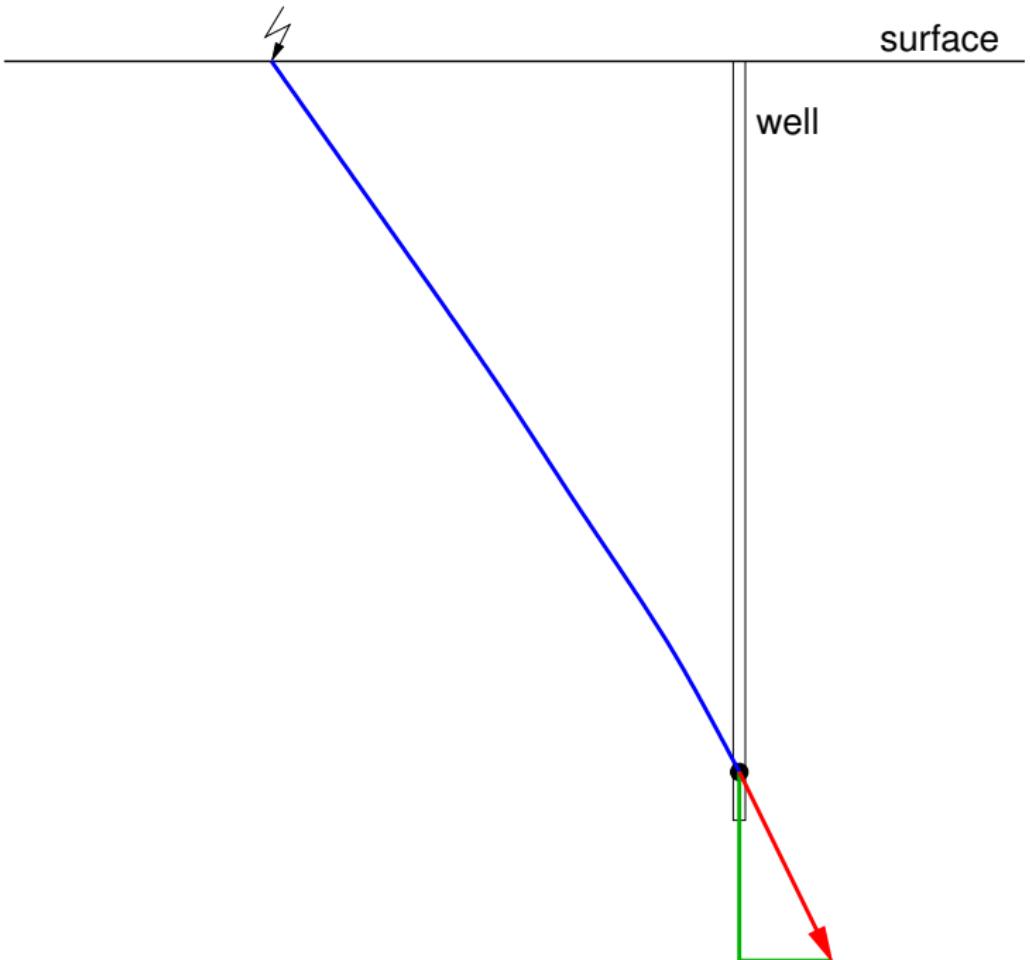
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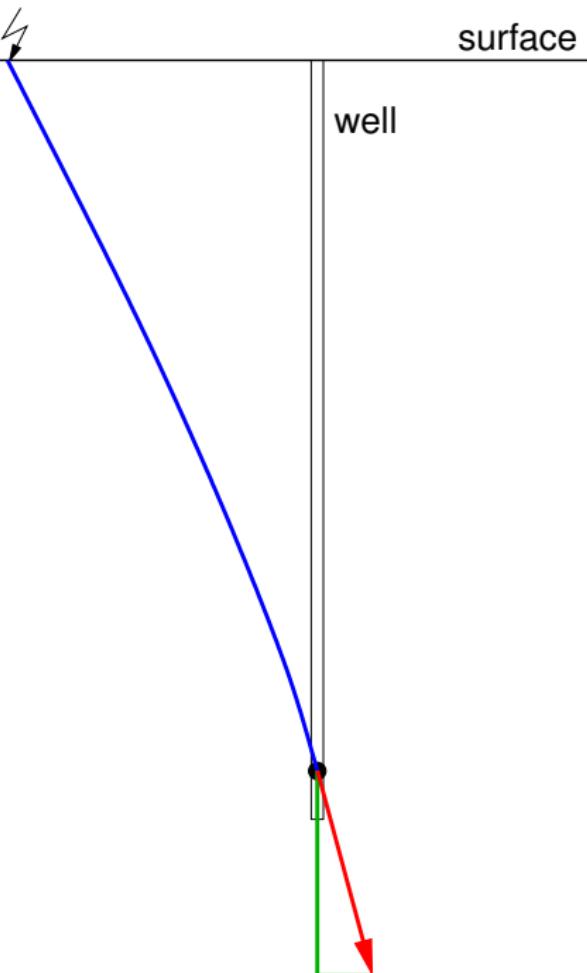
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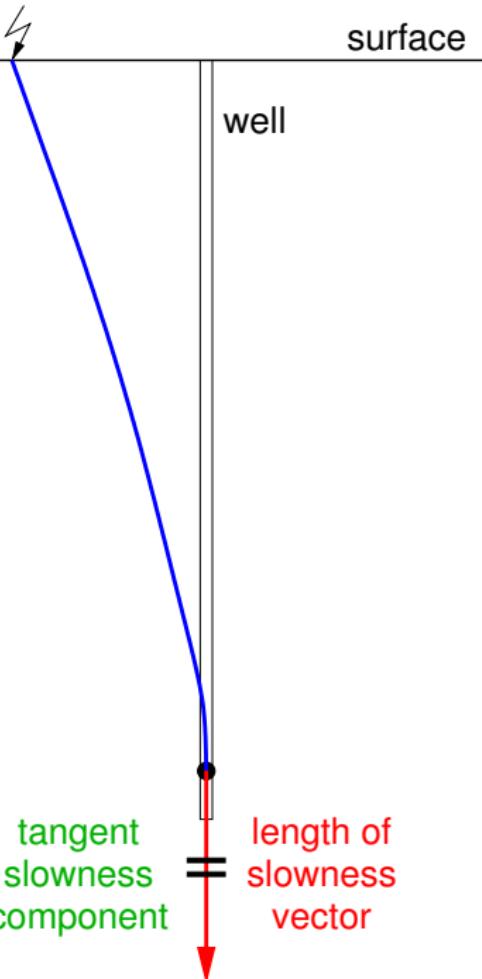
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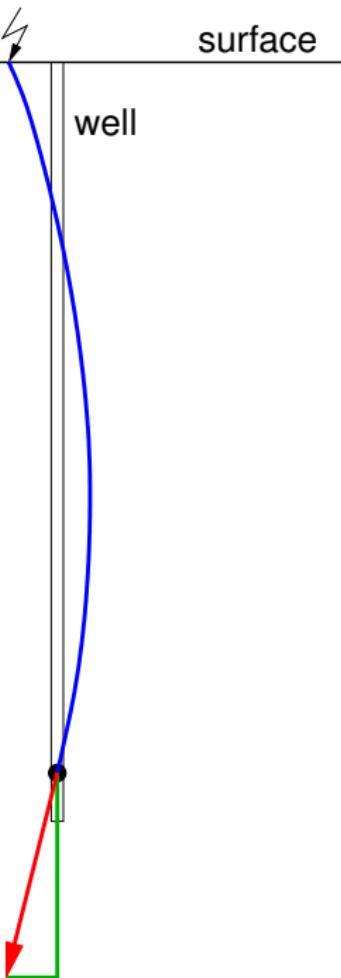
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- ▶ separate calibration for P- and S-waves

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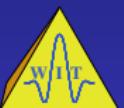
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- ▶ separate calibration for P- and S-waves
- ▶ velocity v_G is property of receiver position

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- ▶ separate calibration for P- and S-waves
- ▶ velocity v_G is property of receiver position
 - ➡ applicable to also calibrate *reflected* waves

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- ▶ Geometric interpretation provides

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 - ▶ redatuming

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- ▶ velocity v_G is property of receiver position
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 - ▶ inversion
- ▶ strategy also suited for deviated wells

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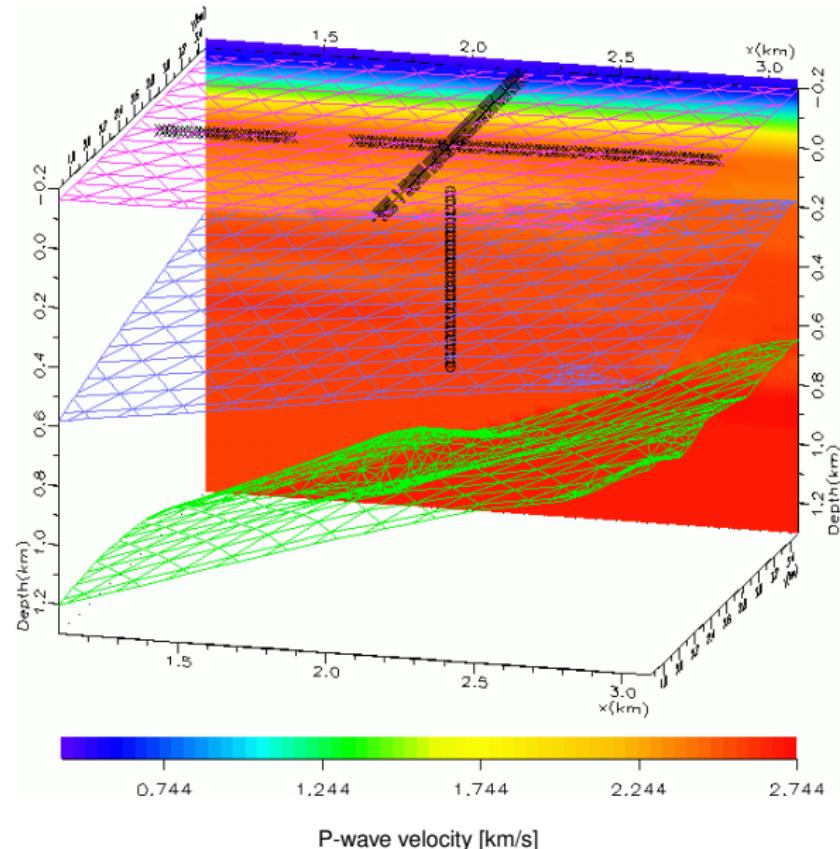
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Modeling:

- ▶ wavefront construction method

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Modeling:

- ▶ wavefront construction method
- ▶ direct P, reflected PP & SS, converted PS

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Modeling:

- ▶ wavefront construction method
- ▶ direct P, reflected PP & SS, converted PS
- ▶ 3D wave propagation

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Modeling:

- ▶ wavefront construction method
- ▶ direct P, reflected PP & SS, converted PS
- ▶ 3D wave propagation
- ▶ two walkover lines, 100 shots each

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Modeling:

- ▶ wavefront construction method
- ▶ direct P, reflected PP & SS, converted PS
- ▶ 3D wave propagation
- ▶ two walkover lines, 100 shots each
- ▶ 40 three-component receiver levels

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Modeling:

- ▶ wavefront construction method
- ▶ direct P, reflected PP & SS, converted PS
- ▶ 3D wave propagation
- ▶ two walkover lines, 100 shots each
- ▶ 40 three-component receiver levels
- ▶ 2D approach sufficiently accurate for calibration

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convenient CRS parameter: emergence angle

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convenient CRS parameter: emergence angle
→ tangency \equiv zero angle

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convenient CRS parameter: emergence angle

→ tangency \equiv zero angle

Expected behavior:

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convenient CRS parameter: emergence angle

→ tangency \equiv zero angle

Expected behavior:

- ▶ over-estimated velocity

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convenient CRS parameter: emergence angle

→ tangency \equiv zero angle

Expected behavior:

- ▶ over-estimated velocity
- zero angle smeared over large offset range

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convenient CRS parameter: emergence angle

→ tangency \equiv zero angle

Expected behavior:

- ▶ over-estimated velocity
zero angle smeared over large offset range
- ▶ under-estimated velocity

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convenient CRS parameter: emergence angle

→ tangency \equiv zero angle

Expected behavior:

- ▶ over-estimated velocity
zero angle smeared over large offset range
- ▶ under-estimated velocity
zero angle never occurs

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convenient CRS parameter: emergence angle

→ tangency ≡ zero angle

Expected behavior:

- ▶ over-estimated velocity
zero angle smeared over large offset range
- ▶ under-estimated velocity
zero angle never occurs
- ▶ correct velocity

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convenient CRS parameter: emergence angle

→ tangency \equiv zero angle

Expected behavior:

- ▶ over-estimated velocity
zero angle smeared over large offset range
- ▶ under-estimated velocity
zero angle never occurs
- ▶ correct velocity
well-localized minimum at zero angle

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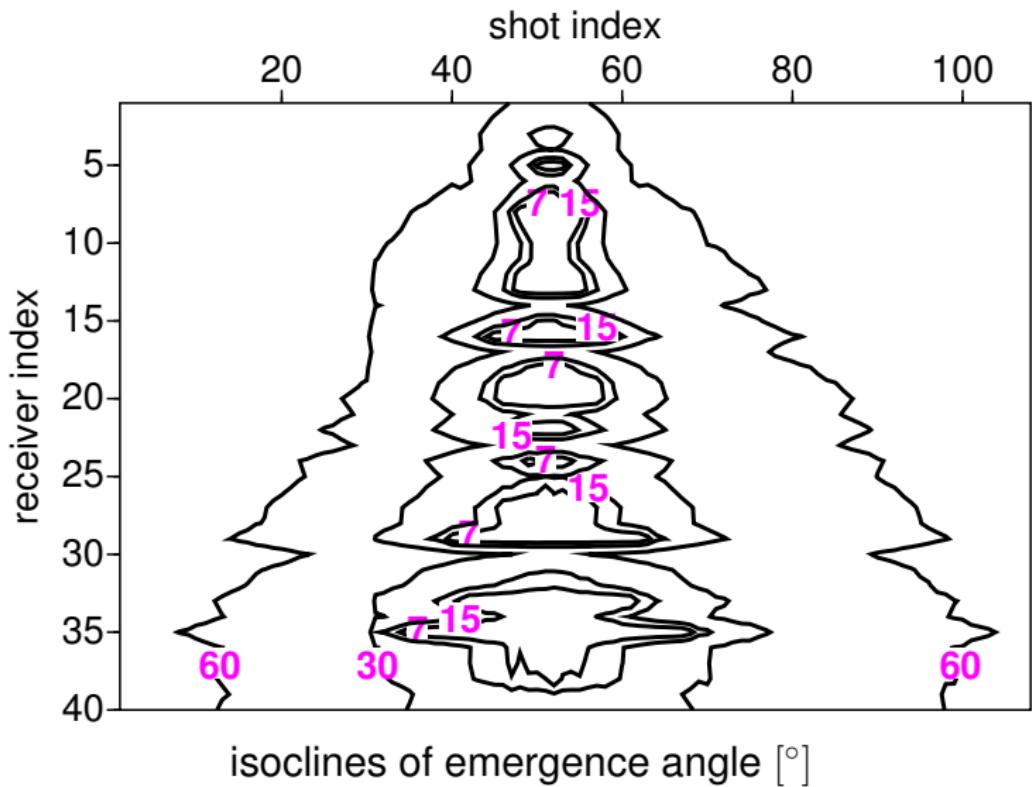
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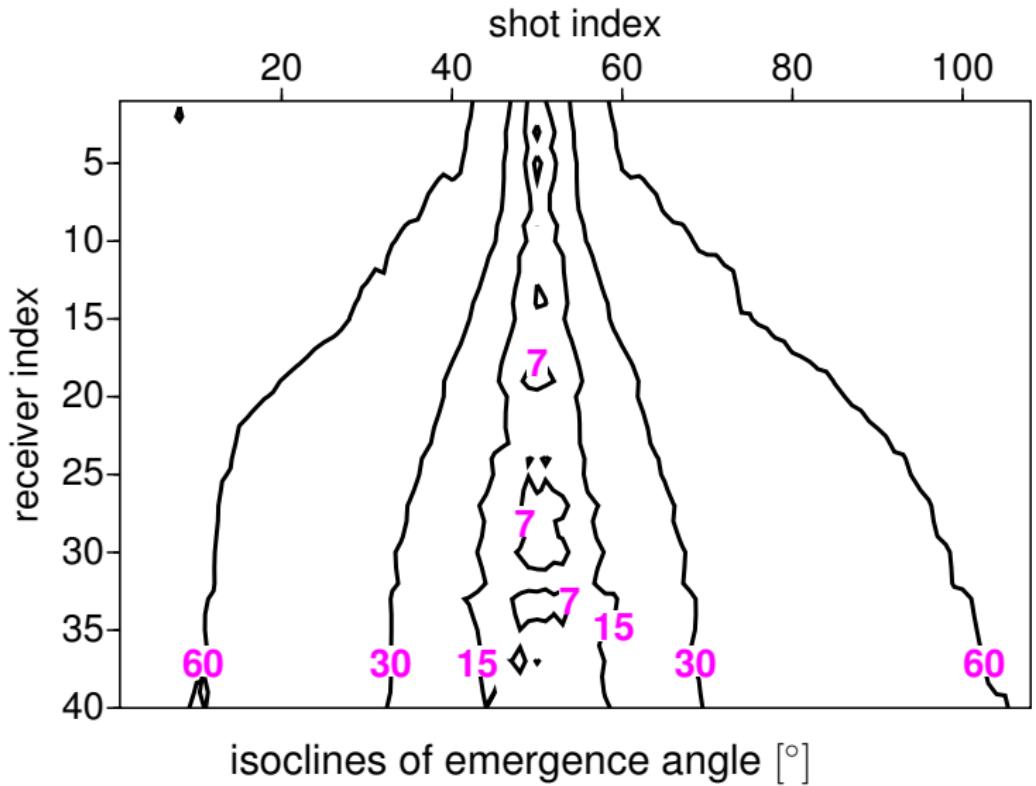
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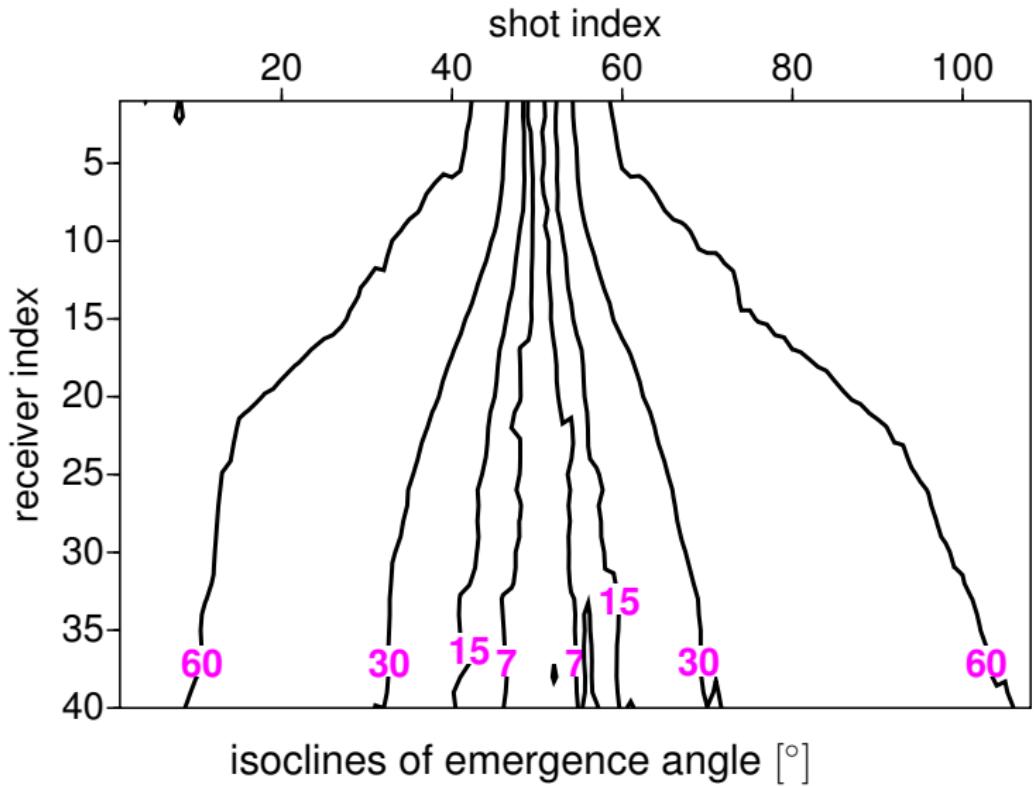
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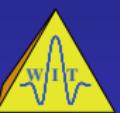
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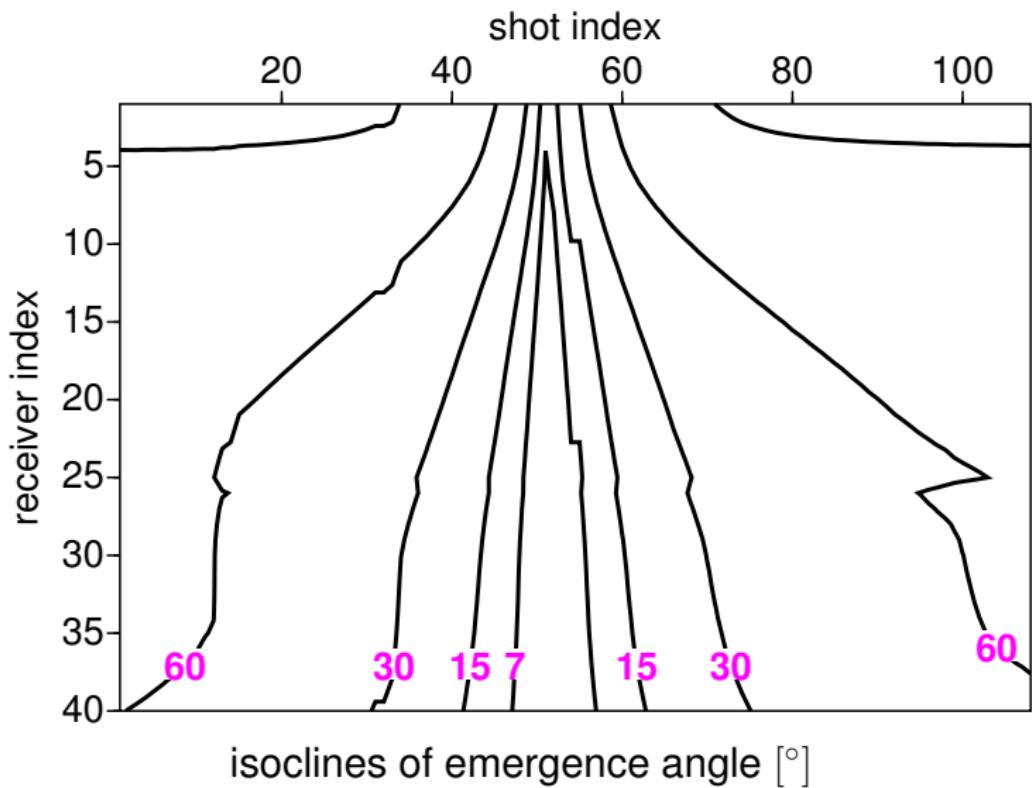
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1D velocity curves along well

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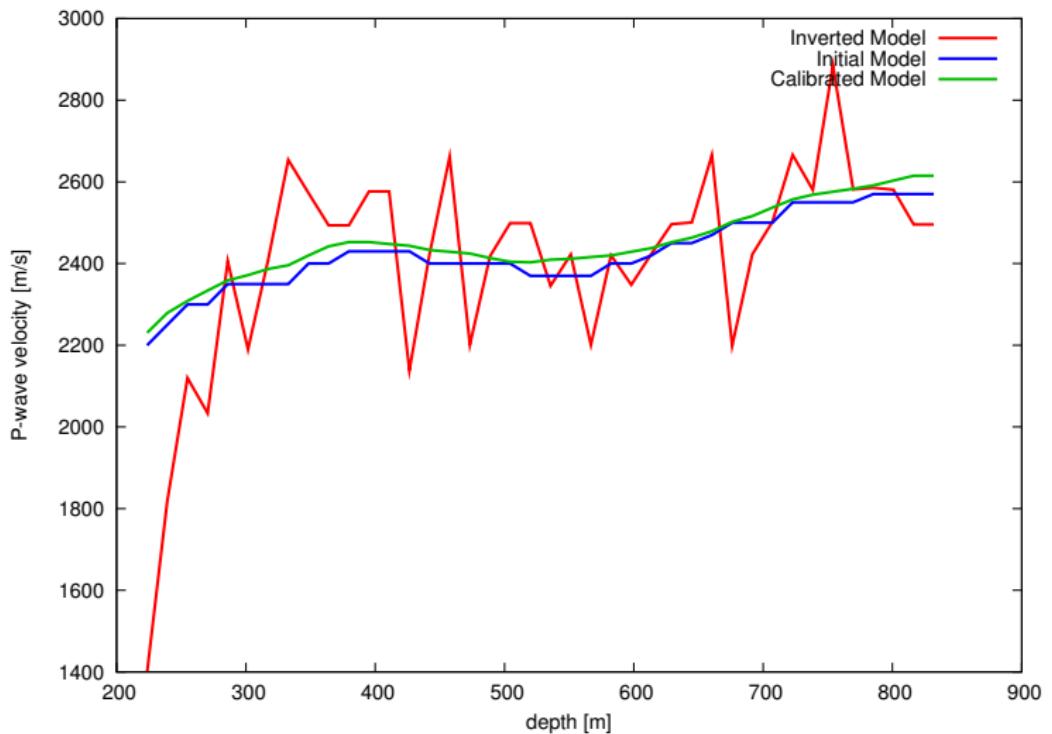
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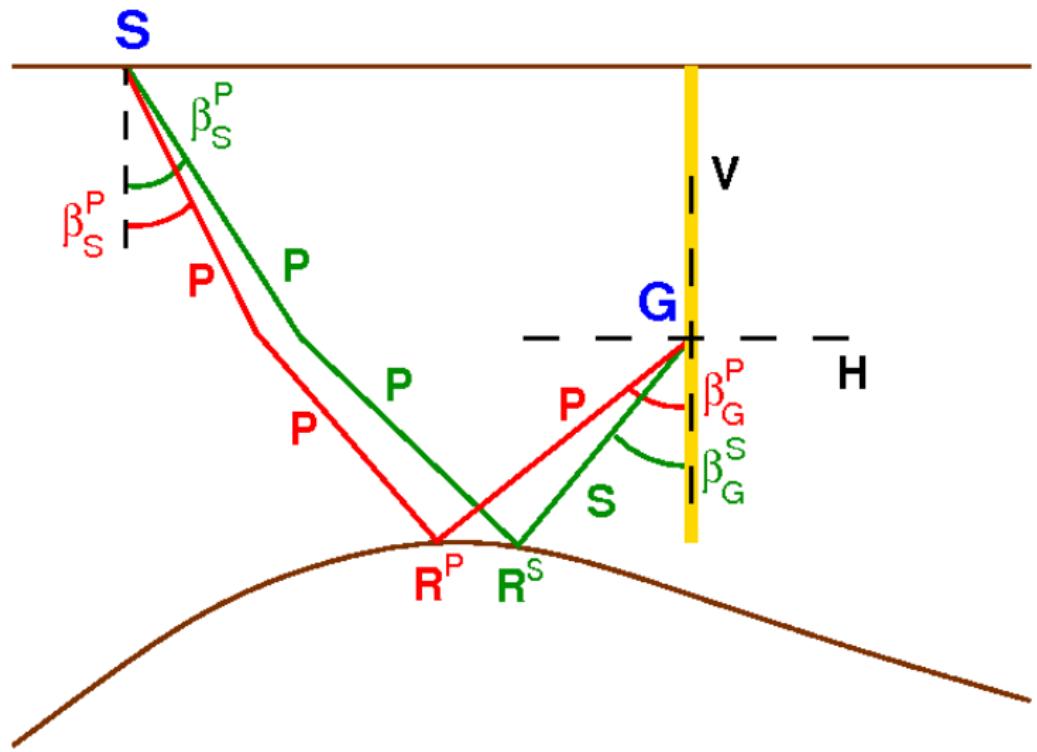
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Components (V,H) prior to rotation

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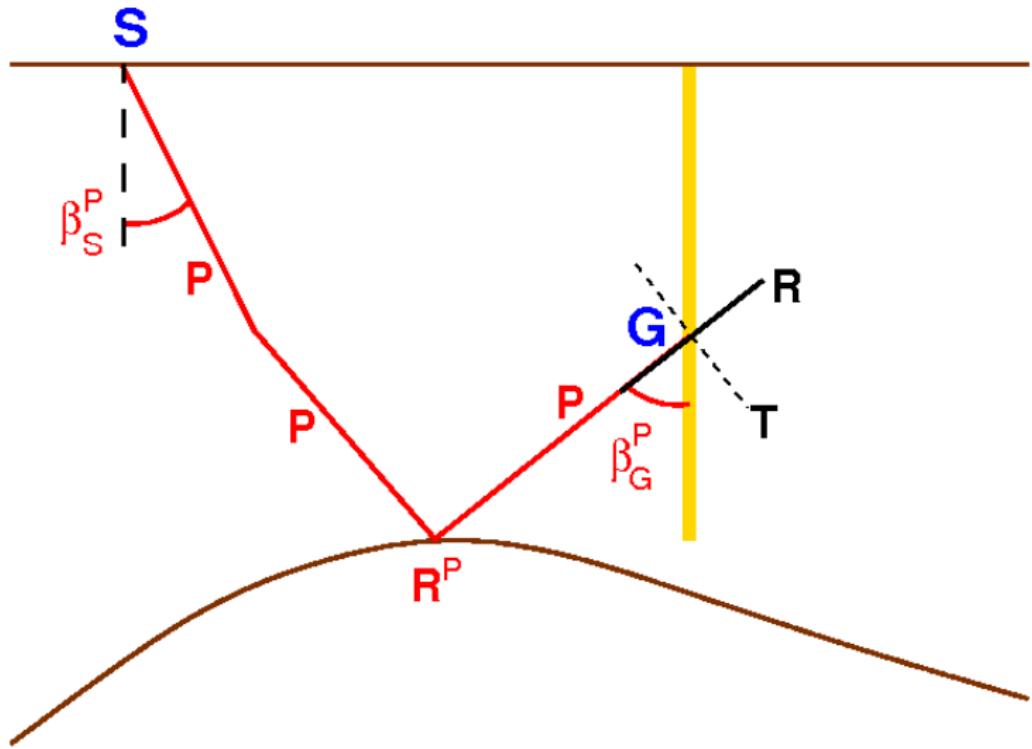
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Components (R,T) after rotation by β_G^P – R is strong

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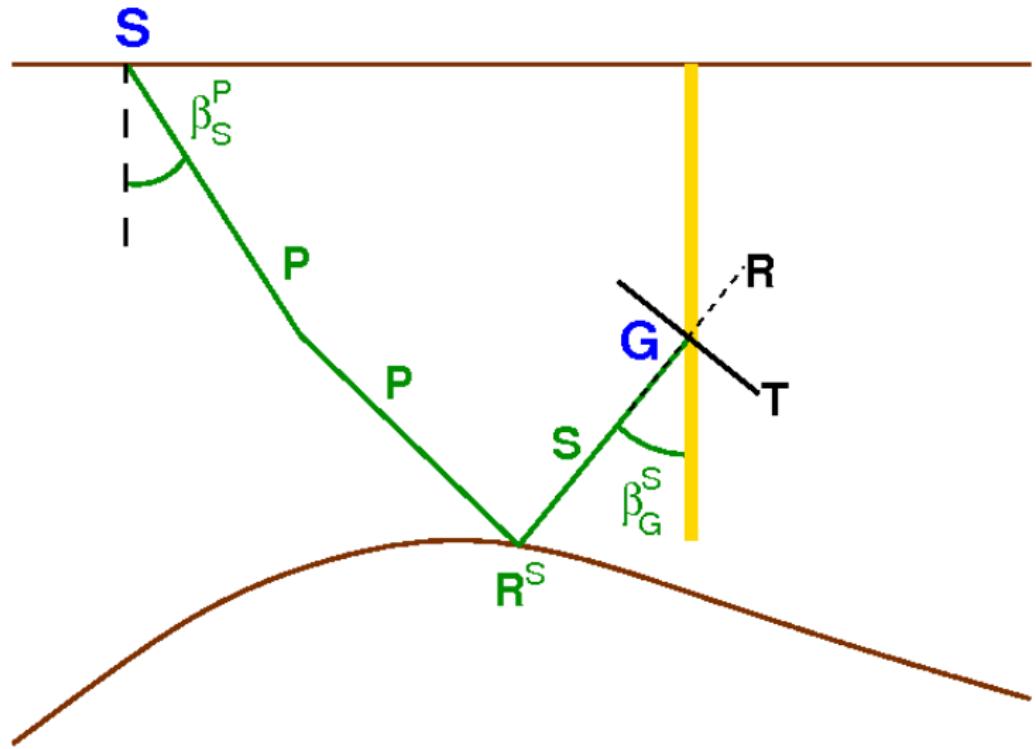
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Components (R,T) after rotation by β_G^S – T is strong

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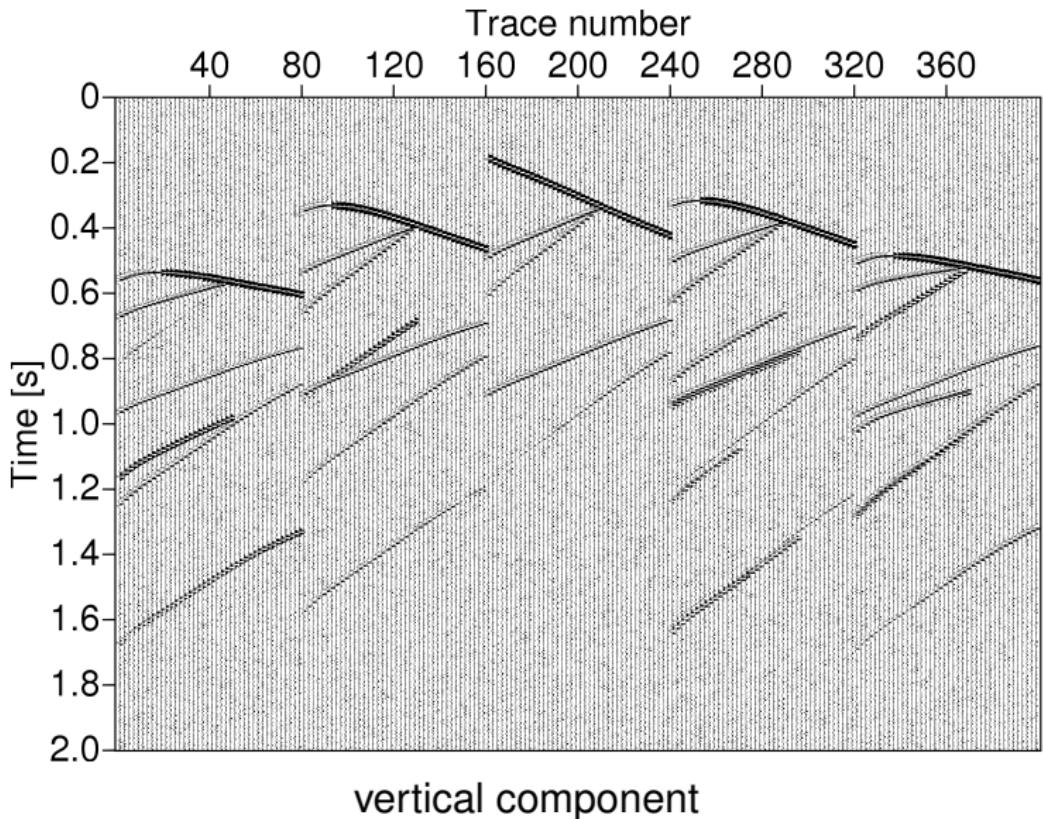
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Five CS gathers prior to rotation



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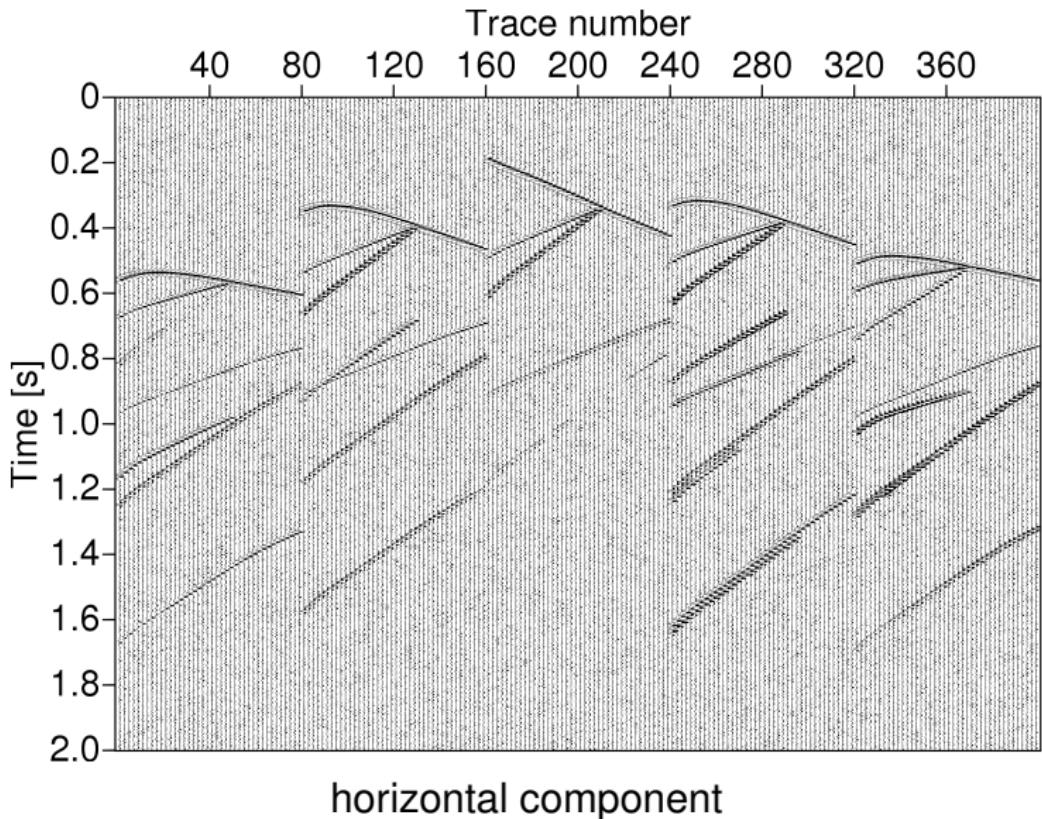
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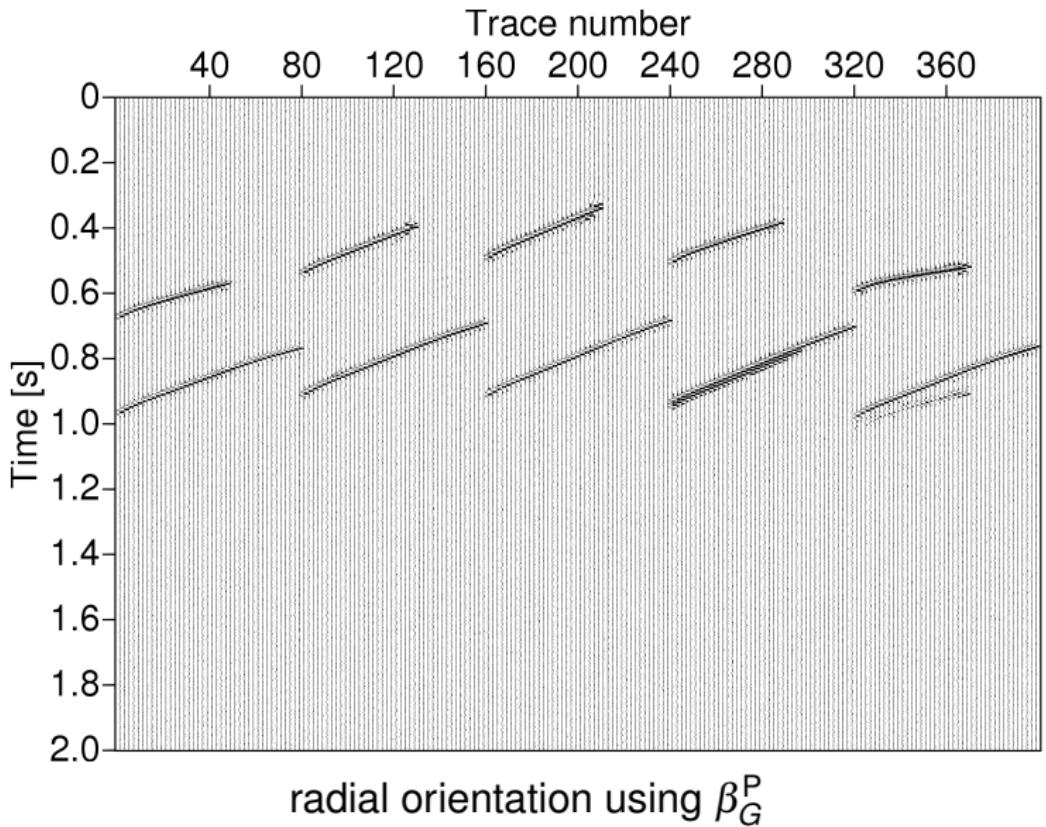
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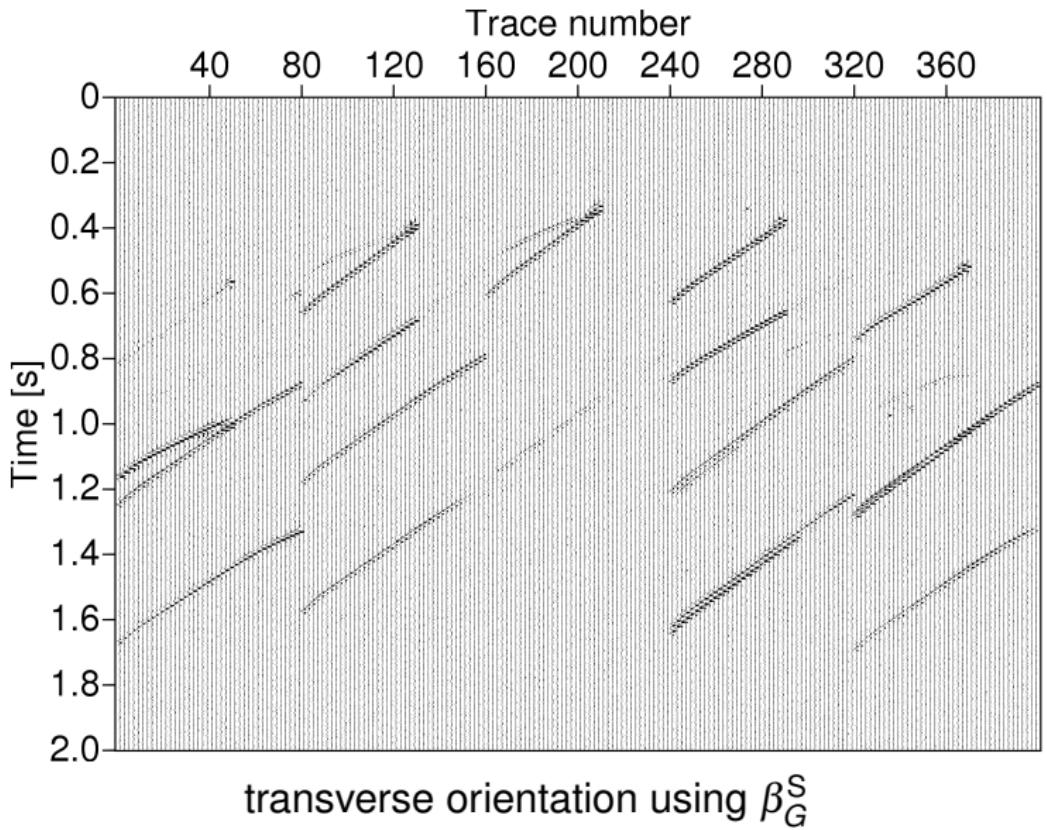
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Calibration of CRS attributes

- ▶ high sensitivity to inaccurate velocity

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Calibration of CRS attributes

- ▶ high sensitivity to inaccurate velocity
- ▶ simple criterion to determine tuned velocities

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Calibration of CRS attributes

- ▶ high sensitivity to inaccurate velocity
- ▶ simple criterion to determine tuned velocities
- ▶ readily applicable to 3D data and deviated wells

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Calibration of CRS attributes

- ▶ high sensitivity to inaccurate velocity
- ▶ simple criterion to determine tuned velocities
- ▶ readily applicable to 3D data and deviated wells
- ▶ reliable *geometrical* CRS attributes for

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